



Electromagnetics

Part 2

Wei E.I. Sha (沙威)

College of Information Science & Electronic Engineering
Zhejiang University, Hangzhou 310027, P. R. China

Email: weisha@zju.edu.cn

Website: <http://www.isee.zju.edu.cn/weisha>

Course Overview

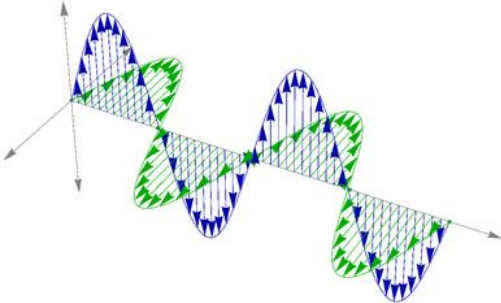
1. Plane Waves
2. Polarization
3. Plane Waves in Multilayer Media
4. Excitation Problem and Eigenvalue Problem
5. Wave Physics

1. Plane Waves (1)

Plane waves (homogeneous and sourceless region)

$$\begin{aligned} \nabla \times \mathbf{E} &= -j\omega \mathbf{B} & \nabla \times \nabla \times \mathbf{E} &= -j\omega \nabla \times \mathbf{B} = \omega^2 \mu \epsilon \mathbf{E} & k &= \omega \sqrt{\mu \epsilon} & \text{wavenumber} \\ \nabla \times \mathbf{H} &= j\omega \mathbf{D} \end{aligned}$$

$$\nabla \times \nabla \times \mathbf{E} - k^2 \mathbf{E} = 0 \quad \nabla \cdot \mathbf{E} = 0 \quad \text{sourceless} \quad \boxed{\nabla^2 \mathbf{E} + k^2 \mathbf{E} = 0}$$



plane wave is an eigenmode of wave equation
(solution of Maxwell equation without excitations)

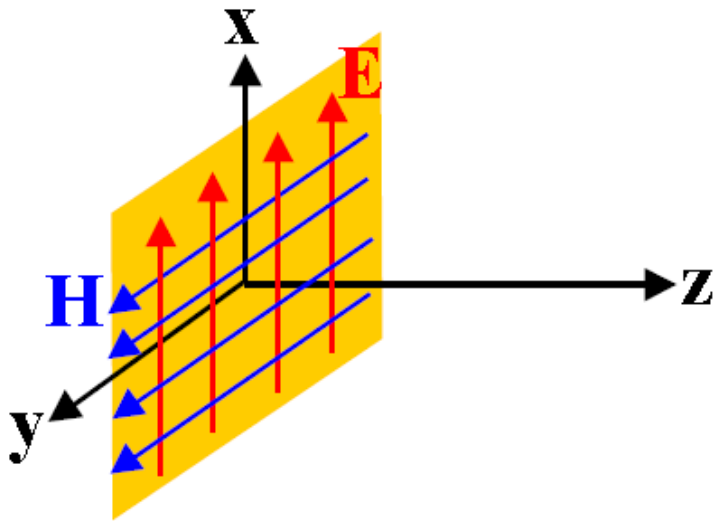
$$\mathbf{E} = E_0 \exp(-jkz) \mathbf{e}_x$$

amplitude
propagation direction
polarization direction

time domain
 $\mathbf{E} = E_0 \operatorname{Re}[\exp(j\omega t) \exp(-jkz)] \mathbf{e}_x$
 $= E_0 \cos(\omega t - kz) \mathbf{e}_x$

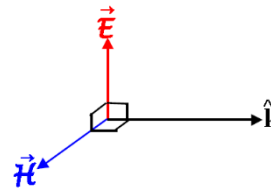
1. Plane Waves (2)

$$\nabla \times \mathbf{E} = -j\omega\mathbf{B} \rightarrow \mathbf{H} = \frac{\nabla \times \mathbf{E}}{-j\omega\mu} = \frac{1}{-j\omega\mu} \frac{\partial E_x}{\partial z} \mathbf{e}_y \rightarrow \eta = \frac{\omega\mu}{k} = \sqrt{\frac{\mu}{\epsilon}}$$
$$= E_0 \frac{k}{\omega\mu} \exp(-jkz) \mathbf{e}_y = \frac{E_0}{\eta} \exp(-jkz) \mathbf{e}_y \quad \text{wave impedance}$$



$$\omega t - k_0 z = C$$

wavefront is defined by setting the phase equal to a constant



$$v_p = \frac{dz}{dt} = \frac{\omega}{k}$$

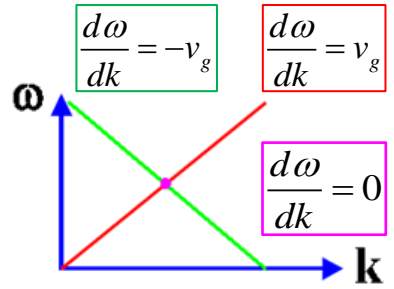
phase velocity

1. Amplitudes of fields on a given constant-phase plane are uniform.
2. In practice, most waves are spherical waves rather than plane waves. But if the observation point is far from the source, it can be approximated as a plane wave.
3. Gauss beam from laser can be approximated as a plane wave.

1. Plane Waves (3)

Propagating waves

$$\mathbf{E} = E_0 \exp(-jkz) \mathbf{e}_x \xrightarrow[\text{domain}]{\text{time}} \mathbf{E} = E_0 \cos(\omega t - kz) \mathbf{e}_x$$

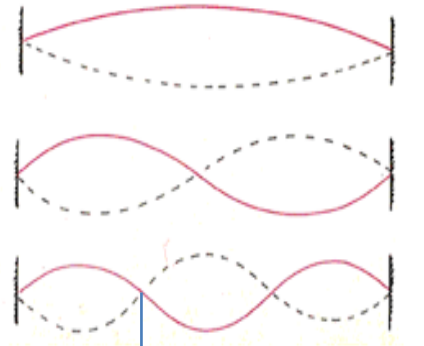


Standing waves

$$\mathbf{E} = 0.5 \left[E_0 \exp(-jkz) \mathbf{e}_x + E_0 \exp(jkz) \mathbf{e}_x \right] \xrightarrow[\text{domain}]{\text{time}} \mathbf{E} = E_0 \cos(\omega t) \cos(kz) \mathbf{e}_x$$

$$= E_0 \cos(kz) \mathbf{e}_x$$

1. Standing waves do not propagate EM energy with zero group velocity.
2. Standing waves relate to eigenmodes of EM resonances.



node antinode

nodal plane ←

Mode shape	<i>m</i>	<i>n</i>	$(\omega/\omega_0)^2$	ω/ω_0
+	1	1	1.25	1.12
+ -	1	2	2.00	1.41
+ - +	1	3	3.25	1.80
- +	2	1	4.25	2.06
- + + -	2	2	5.00	2.24

2. Polarization

The curve traced out by the tip of \mathbf{E} at a fixed point in space as time t varies

linearly polarized : locus is a straight line

circularly polarized : locus is a circle

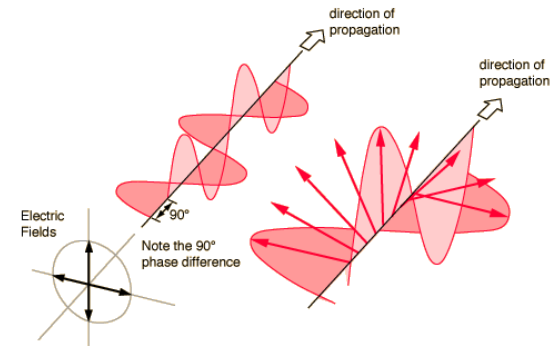
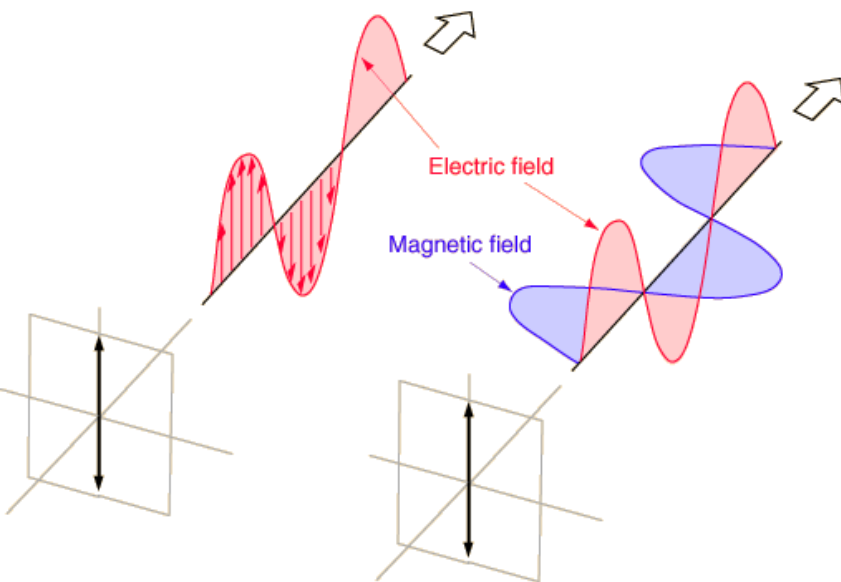
elliptically polarized : locus is an ellipse

unpolarized : superposition of linearly polarized waves with random orientations (Sunlight).

right-circularly polarized

$$\mathbf{E} = (\mathbf{e}_x - j\mathbf{e}_y) E_0 \exp(-jkz)$$

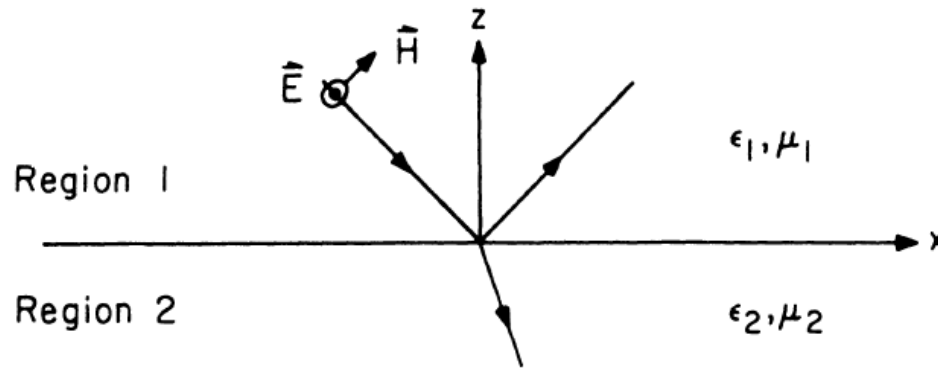
linear polarized



If looking at the source, electric vector coming toward you is rotating counterclockwise, the wave is right-circularly polarized. If clockwise, it is left-circularly polarized.

3. Plane Waves in Multilayer Media (1)

Reflection and transmission of a plane wave at an interface



TE waves $E_y = e_y(z)e^{-jk_x x}$ $e_{1y}(z) = e_0 \exp(jk_{1z}z) + R^{TE} e_0 \exp(-jk_{1z}z)$

$$\begin{aligned}
 E_{1t} = E_{2t} & \qquad 1 + R^{TE} = T^{TE} \\
 H_{1t} = H_{2t} & \longrightarrow \frac{k_{1z}}{\mu_1} (1 - R^{TE}) = \frac{k_{2z}}{\mu_2} T^{TE} \longrightarrow
 \end{aligned}$$

$$\begin{aligned}
 R^{TE} &= \frac{\mu_2 k_{1z} - \mu_1 k_{2z}}{\mu_2 k_{1z} + \mu_1 k_{2z}} \\
 T^{TE} &= \frac{2\mu_2 k_{1z}}{\mu_2 k_{1z} + \mu_1 k_{2z}}
 \end{aligned}$$

$$\begin{aligned}
 R^{TM} &= \frac{\epsilon_2 k_{1z} - \epsilon_1 k_{2z}}{\epsilon_2 k_{1z} + \epsilon_1 k_{2z}} \\
 T^{TM} &= \frac{2\epsilon_2 k_{1z}}{\epsilon_2 k_{1z} + \epsilon_1 k_{2z}}
 \end{aligned}$$

3. Plane Waves in Multilayer Media (2)

1. If $k_1 > k_2$, there exist values of k_x such that $k_1 > k_x > k_2$, implying that k_{2z} is purely imaginary, while k_{1z} is purely real. Hence, the magnitude of R_{TE} or R_{TM} equals 1. In other words, all the energy of the incident wave is reflected. This phenomenon is known as *total internal reflection*.

2. there exist values of k_x such that R_{TE} or R_{TM} equals zero. Then, the corresponding angle for which the reflection coefficient equals zero is known as the *Brewster angle*. Brewster angle effect is more prevalent for TM waves because most materials are nonmagnetic.

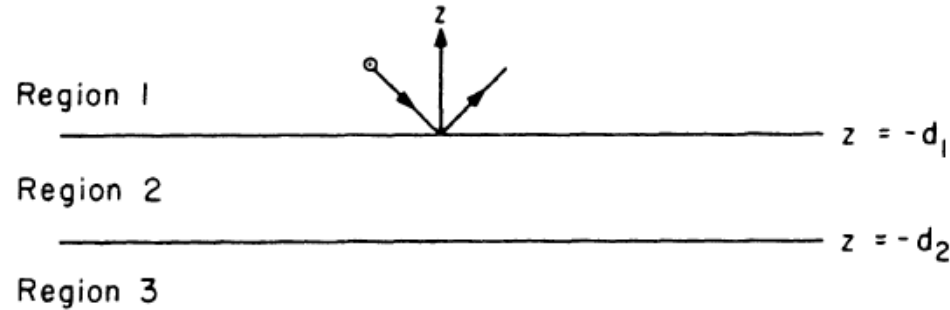
3. The poles of the reflection coefficients relate to dispersion relation of the multilayer system. (For eigenvalue problem, we have the nonzero reflection field with a zero incident field/excitation!)

$$\text{TM wave} \quad \varepsilon_2 k_{1z} + \varepsilon_1 k_{2z} = 0 \quad \varepsilon_2 \sqrt{k_1^2 - k_x^2} + \varepsilon_1 \sqrt{k_2^2 - k_x^2} = 0$$

$$k_x = k_0 \sqrt{\frac{\varepsilon_1 \varepsilon_2}{\varepsilon_1 + \varepsilon_2}} \quad \text{dispersion of surface plasmon!}$$

3. Plane Waves in Multilayer Media (3)

Reflection from a three-layer medium



wave in region 1

$$e_{1y} = A_1 [\exp(jk_{1z}z) + \tilde{R}_{12} \exp(-2jk_{1z}d_1 - jk_{1z}z)]$$

generalized reflection coefficient

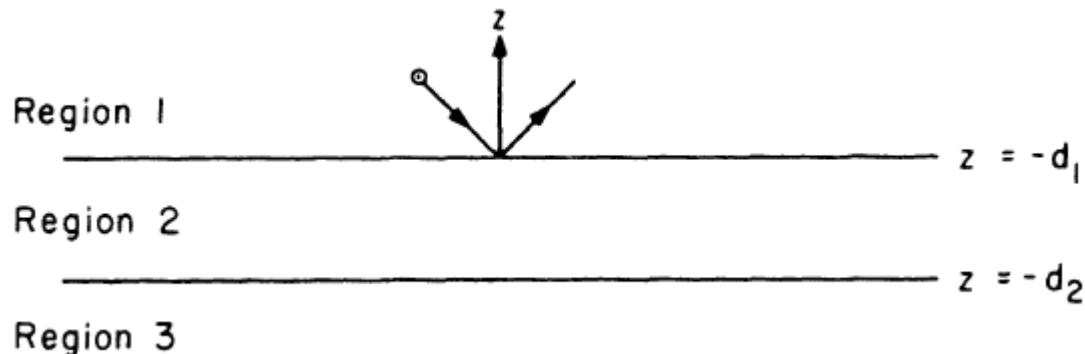
wave in region 2

$$e_{2y} = A_2 [\exp(jk_{2z}z) + R_{23} \exp(-2jk_{2z}d_2 - jk_{2z}z)]$$

wave in region 3

$$e_{3y} = A_3 \exp(jk_{3z}z)$$

3. Plane Waves in Multilayer Media (4)



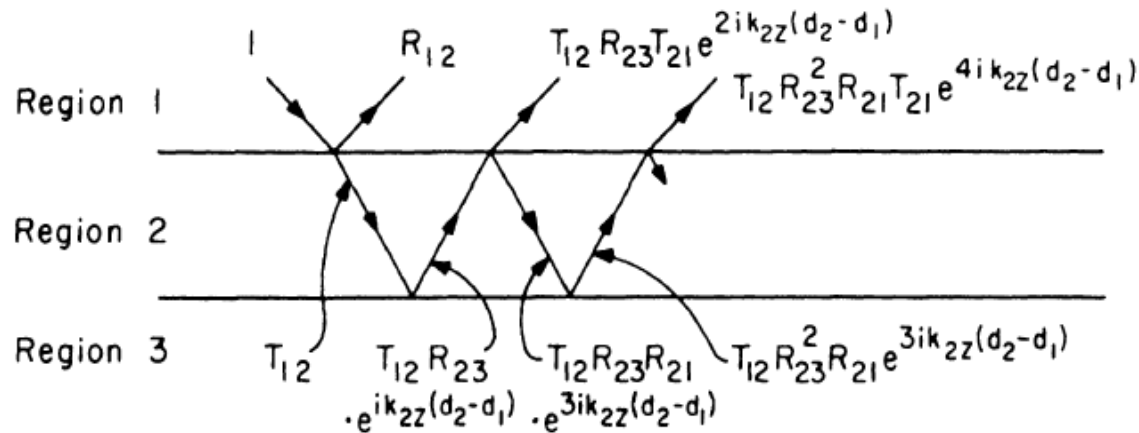
1. Downgoing wave in region 2 is a consequence of the transmission of downgoing wave in region 1 plus a reflection of upgoing wave in region 2 (at interface of $-d_1$)

$$A_2 \exp(-jk_{2z}d_1) = A_1 \exp(-jk_{1z}d_1)T_{12} + R_{21}A_2R_{23} \exp(-2jk_{2z}d_2 + jk_{2z}d_1)$$

2. Upgoing wave in region 1 is caused by the reflection of downgoing wave in region 1 plus a transmission of upgoing wave in region 2 (at interface of $-d_1$)

$$A_1 \tilde{R}_{12} \exp(-jk_{1z}d_1) = R_{12}A_1 \exp(-jk_{1z}d_1) + T_{21}A_2R_{23} \exp(-2jk_{2z}d_2 + jk_{2z}d_1)$$

3. Plane Waves in Multilayer Media (5)

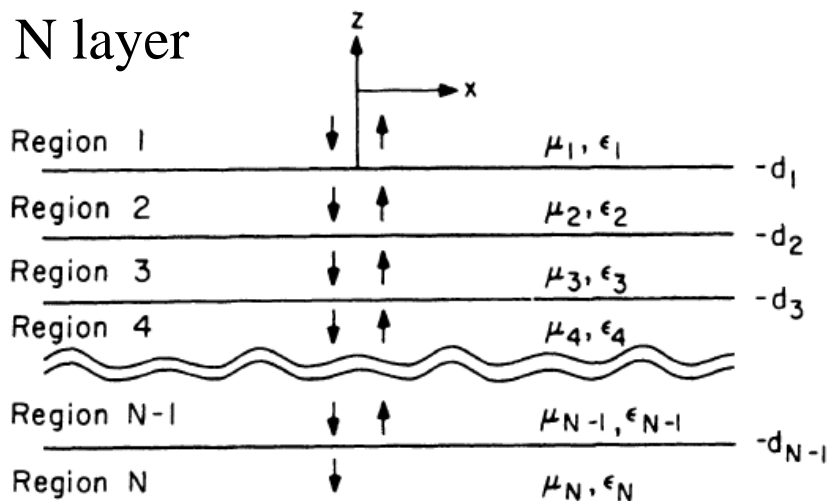


$$i=-j$$

$$\tilde{R}_{12} = R_{12} + \frac{T_{12}R_{23}T_{21} \exp[-2jk_{2z}(d_2 - d_1)]}{1 - R_{21}R_{23} \exp[-2jk_{2z}(d_2 - d_1)]}$$

$$\begin{aligned} \tilde{R}_{12} = & R_{12} + T_{12}R_{23}T_{21} \exp[-2jk_{2z}(d_2 - d_1)] \\ & + T_{12}R_{23}^2R_{21}T_{21} \exp[-4jk_{2z}(d_2 - d_1)] + \dots \end{aligned}$$

3. Plane Waves in Multilayer Media (6)



$$\tilde{R}_{12} = R_{12} + \frac{T_{12} R_{23} T_{21} \exp[-2jk_{2z}(d_2 - d_1)]}{1 - R_{21} R_{23} \exp[-2jk_{2z}(d_2 - d_1)]}$$

generalized

$$\tilde{R}_{i,i+1} = R_{i,i+1} + \frac{T_{i,i+1} \tilde{R}_{i+1,i+2} T_{i+1,i} \exp[-2jk_{i+1,z}(d_{i+1} - d_i)]}{1 - R_{i+1,i} \tilde{R}_{i+1,i+2} \exp[-2jk_{i+1,z}(d_{i+1} - d_i)]}$$

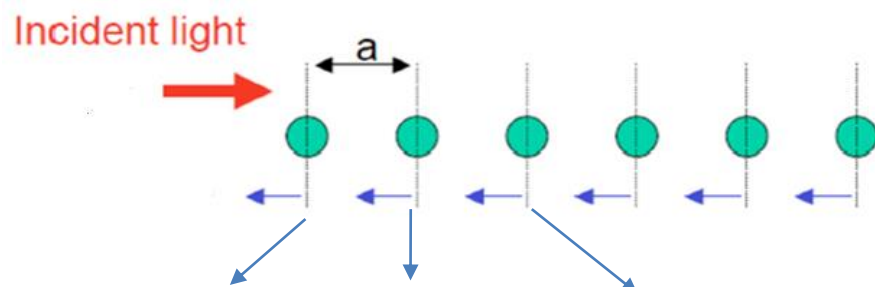
Recursive equation for generalized reflection coefficient

$$R_{i,j} = -R_{j,i} \quad T_{i,j} = 1 + R_{i,j} \quad (\text{See Slide 7})$$

$$\tilde{R}_{i,i+1} = \frac{R_{i,i+1} + \tilde{R}_{i+1,i+2} \exp[-2jk_{i+1,z}(d_{i+1} - d_i)]}{1 + R_{i+1,i} \tilde{R}_{i+1,i+2} \exp[-2jk_{i+1,z}(d_{i+1} - d_i)]} \quad \tilde{R}_{N,N+1} = 0$$

3. Plane Waves in Multilayer Media (7)

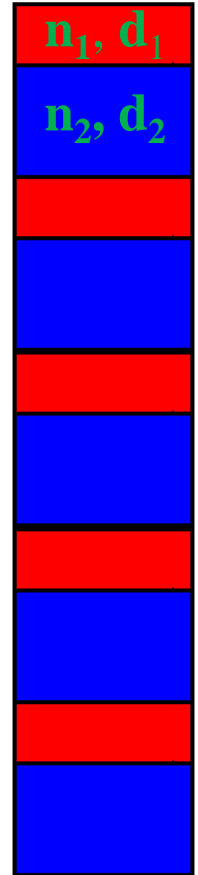
Distributed Bragg reflector



$$\begin{aligned}\tilde{R} &= R + (1-R)Re^{-2jka} + (1-R)^2 Re^{-4jka} + \dots \\ &= \frac{R}{1 - (1-R)e^{-2jka}}\end{aligned}$$

when $\exp(-2jka)=1$, generalized reflection coefficient will equal to 1 due to constructive interference. Bragg condition is $\mathbf{a}=\lambda/2$. Here we ignore the secondary reflection/transmission. The above can be generalized to 1D multilayer media, i.e.

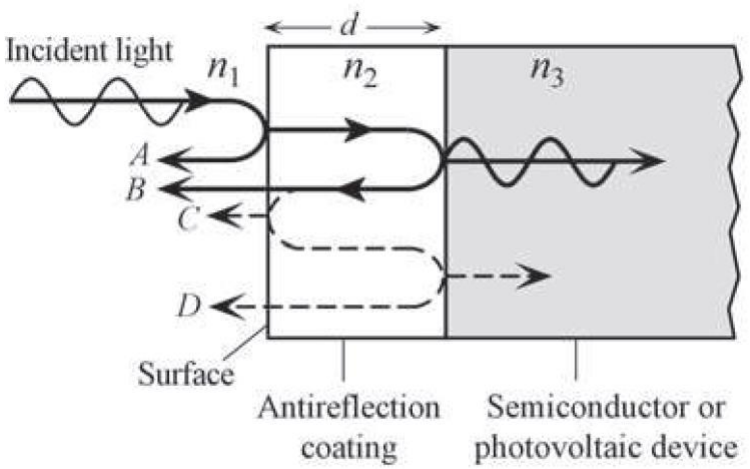
$$\mathbf{n}_1\mathbf{d}_1+\mathbf{n}_2\mathbf{d}_2=\lambda/2.$$



5 periods

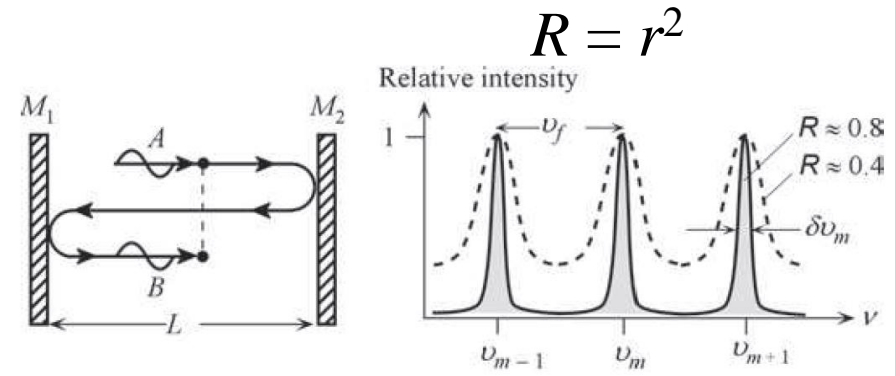
3. Plane Waves in Multilayer Media (8)

More Interference Cases: Antireflection Coatings and Fabry-Perot mode



$$k_2(2d) = \pi$$

$$d = m \left(\frac{\lambda}{4n_2} \right) \quad m = 1, 3, 5, \dots$$



$$k_0(2L) = 2\pi$$

$$m \left(\frac{\lambda}{2} \right) = L; \quad m = 1, 2, 3, \dots$$

$$E_{\text{cavity}} = A + B + \dots = A + Ar^2 \exp(-j2kL) + Ar^4 \exp(-j4kL) + Ar^6 \exp(-j6kL) + \dots$$

$$E_{\text{cavity}} = \frac{A}{1 - r^2 \exp(-j2kL)}$$

4. Excitation Problem and Eigenvalue Problem (1)

Eigenvalue problem

$$\nabla \times \nabla \times \mathbf{F}_m(\mathbf{r}) - k_m^2 \mathbf{F}_m(\mathbf{r}) = 0$$

Excitation problem

$$\nabla \times \nabla \times \mathbf{E}(\mathbf{r}) - k_0^2 \mathbf{E}(\mathbf{r}) = i\omega\mu\mathbf{J}(\mathbf{r})$$

How to connect excitation problem with eigenvalue problem?

eigenmode expansion

$$\mathbf{E}(\mathbf{r}) = \sum_m a_m \mathbf{F}_m(\mathbf{r})$$

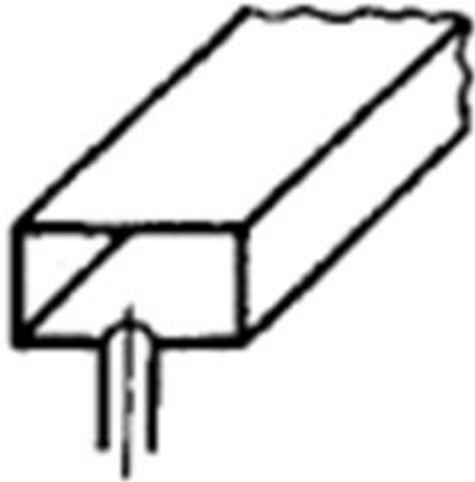
mode orthogonality

$$\int_V d\mathbf{r} \mathbf{F}_{m'}^*(\mathbf{r}) \mathbf{F}_m(\mathbf{r}) = \delta_{m'm}$$

$$\sum_m a_m (k_m^2 - k_0^2) \mathbf{F}_m(\mathbf{r}) = i\omega\mu\mathbf{J}(\mathbf{r})$$

$$a_m = i\omega\mu \frac{\langle \mathbf{F}_m^*, \mathbf{J} \rangle}{k_m^2 - k_0^2}$$

4. Excitation Problem and Eigenvalue Problem (2)



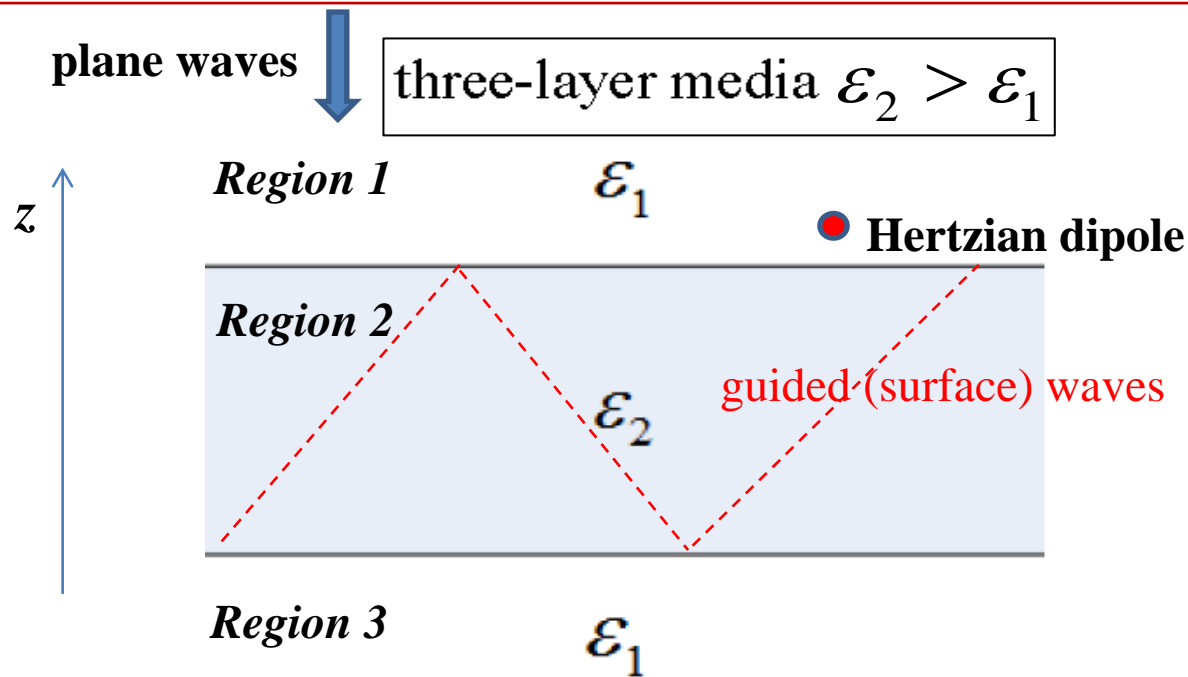
To excite TE_{10} mode of rectangular waveguide

- a. Probe is vertically oriented
- b. Probe is located at the center of bottom side

Please give me a reason.

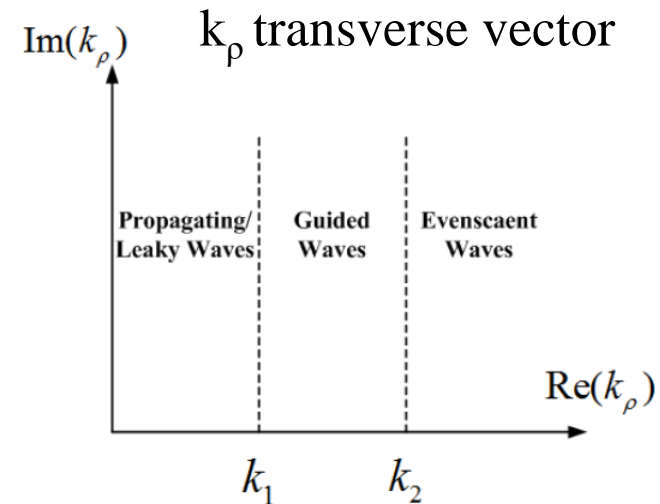
1. The above expression tells us if we want a certain mode to be strongly excited, we need the inner product of the mode and current to be large. Hence, the current on the probe should be located at where the field of the mode is strong. If the probe is a short wire, it can be approximated by an electric dipole and its polarization should be align to that of eigenmode.
2. If the operating frequency of the source is closed to the resonant frequency of the mode, that mode will be strongly excited. This is the phenomenon of resonance coupling. (waveguide here is not a resonator)

5. Wave Physics (1)



$$k_\rho^2 + k_{z1}^2 = k_1^2 \quad \text{Region 1 and 3}$$

$$k_\rho^2 + k_{z2}^2 = k_2^2 \quad \text{Region 2}$$



1. Why a plane wave from region 1 cannot excite guided wave propagating in region 2?

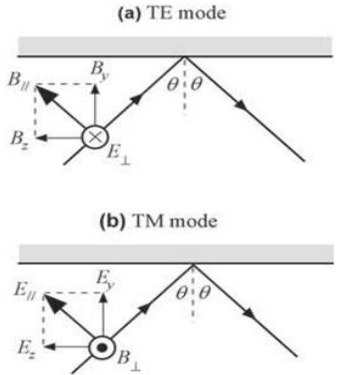
Wavenumber of plane wave is smaller than propagation constant of the guided wave (phase mismatch).

2. Why a Hertzian dipole from region 1 could excite guided waves?

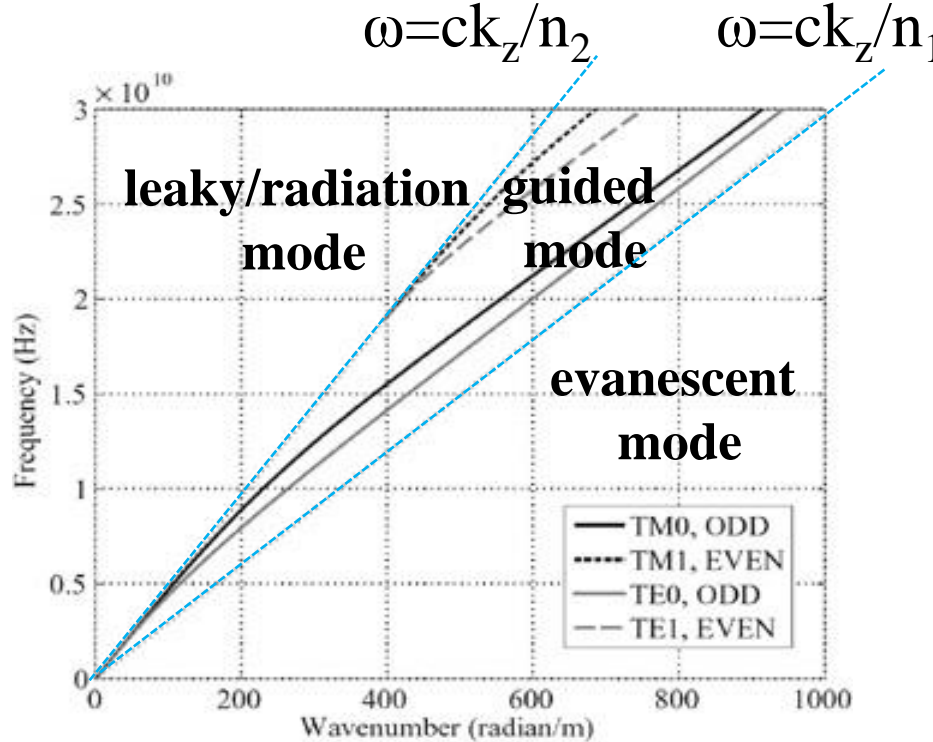
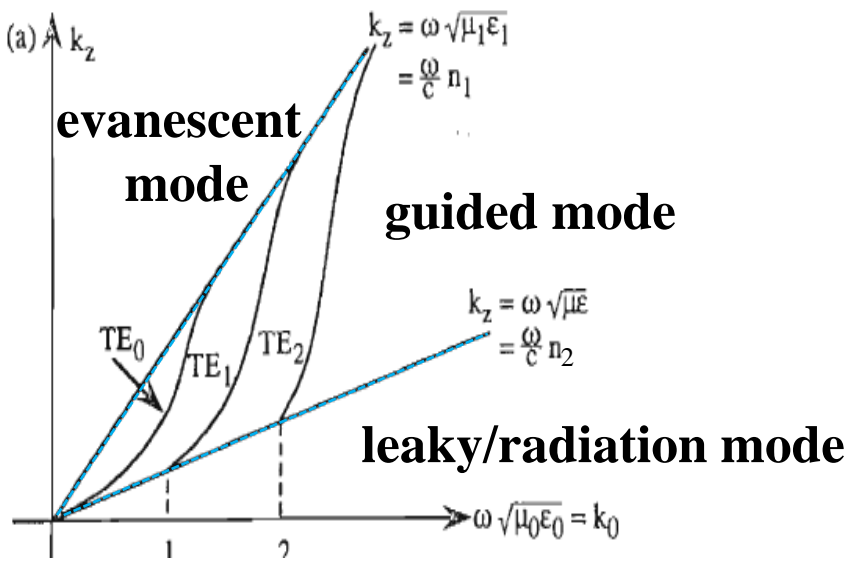
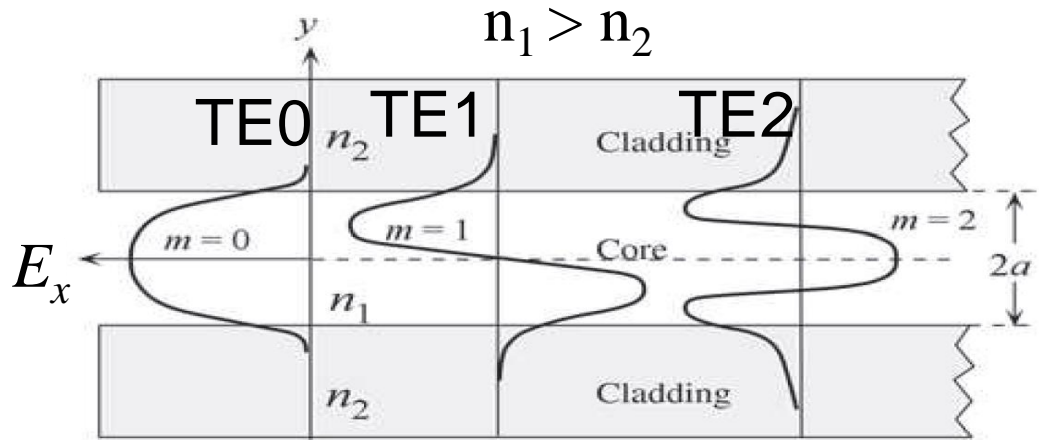
Hertzian dipole with rich evanescent wave components could excite the guided wave if it is near from the interface.

5. Wave Physics (2)

Guided Mode



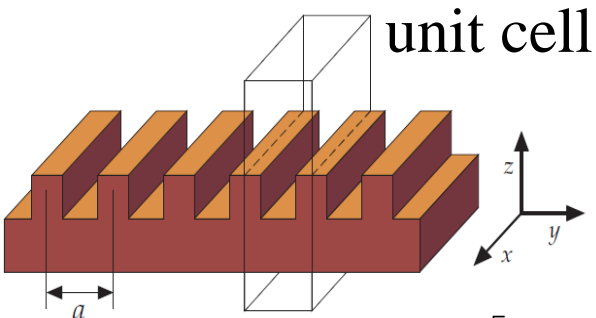
z →



5. Wave Physics (3)

Periodic Grating: We still have continuous translational symmetry in the x direction, but now we have discrete translational symmetry in the y direction

Floquet/Bloch mode

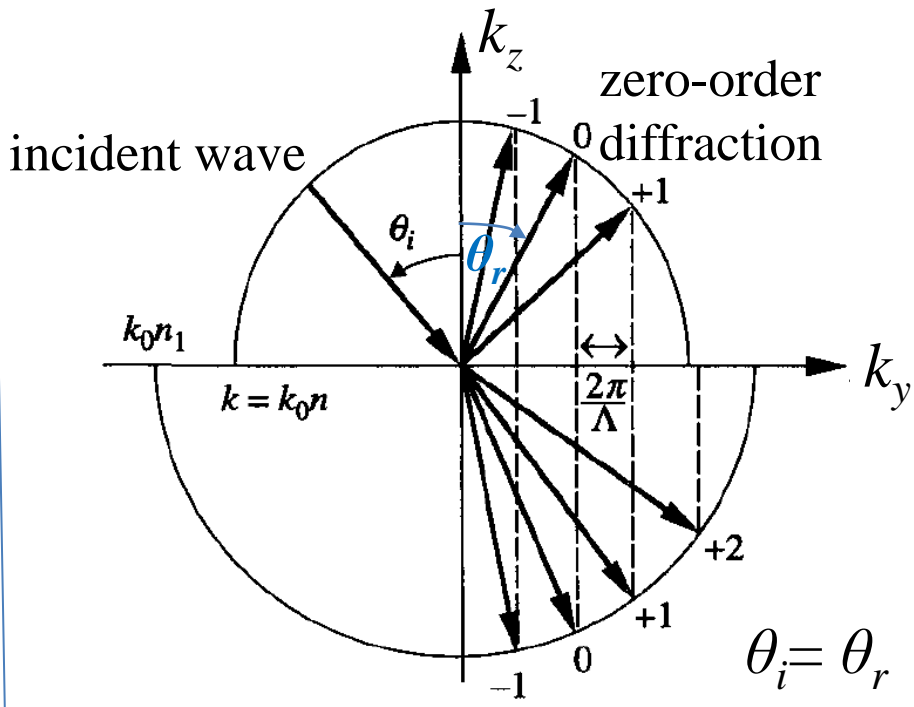


lattice constant

$$\begin{aligned}
 T_R \exp[i(k_y + 2\pi m/a)y] \\
 &= \exp[i(k_y + 2\pi m/a)(y - la)] \\
 &= \exp[i(k_y + 2\pi m/a)y] \exp[-ik_y la]
 \end{aligned}$$

all of the modes with wave vectors of the form $k_y + m(2\pi/a)$, where m is an integer, form a degenerate set; they all have the same eigenvalues of T_R .

phase matching condition



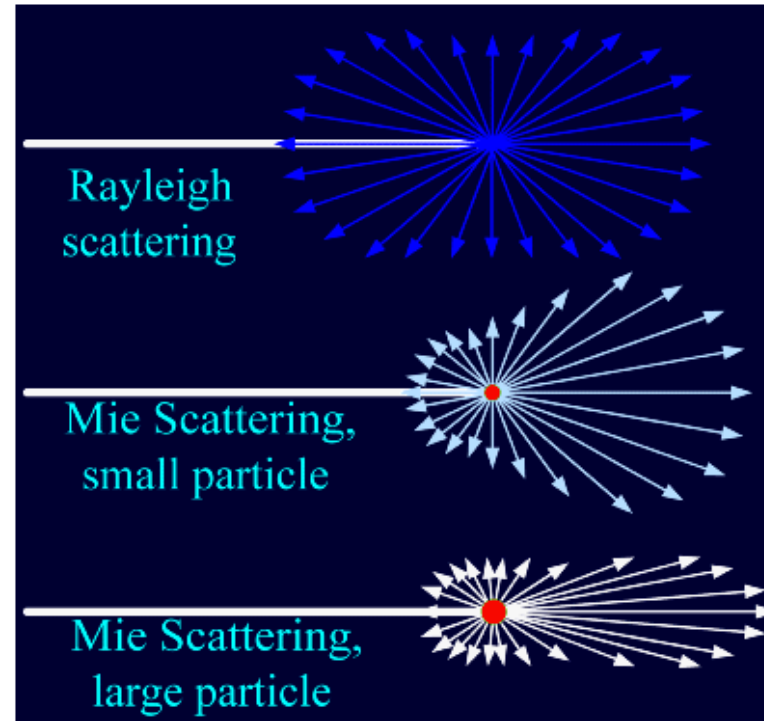
5. Wave Physics (4)

Particle scattering (Optional)

blue sky



sunset



particle
size
from
small
to
large

Rayleigh scattering $\sim 1/\lambda^4$

Mie scattering \sim rely little on wavelength