

Compact Nonlinear Yagi-Uda Nanoantennas

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Supporting Information

Supplementary Note 1: Multipole Expansion for Equivalent Currents

According to Huygens' principle, electric field can be represented by the Green's tensor $\overline{\mathbf{G}}$

$$\mathbf{E} = i\omega\mu \int \overline{\mathbf{G}}(\mathbf{r}, \mathbf{r}') \cdot \mathbf{J}(\mathbf{r}') d\mathbf{r}' - \int \nabla \times \overline{\mathbf{G}}(\mathbf{r}, \mathbf{r}') \cdot \mathbf{M}(\mathbf{r}') d\mathbf{r}' \quad (1)$$

where $\overline{\mathbf{G}}(\mathbf{r}, \mathbf{r}') = (\overline{\mathbf{I}} + \frac{\nabla\nabla}{k^2})g(\mathbf{r}, \mathbf{r}')$ and $g(\mathbf{r}, \mathbf{r}') = \frac{\exp(ik|\mathbf{r}-\mathbf{r}'|)}{4\pi|\mathbf{r}-\mathbf{r}'|}$.

In the far-field region ($kr \gg 1$), it is sufficient to approximate

$$|\mathbf{r} - \mathbf{r}'| \approx r - \hat{\mathbf{r}} \cdot \mathbf{r}' \quad (2)$$

Then electric field is

$$\begin{aligned} \mathbf{E} &= i\omega\mu \frac{e^{ikr}}{4\pi r} \left(\hat{\theta}\hat{\theta} + \hat{\phi}\hat{\phi} \right) \cdot \int \mathbf{J}(\mathbf{r}') e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} d\mathbf{r}' - ik \frac{e^{ikr}}{4\pi r} \hat{\mathbf{r}} \times \int \mathbf{M}(\mathbf{r}') e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} d\mathbf{r}' \\ &= ik\eta \frac{e^{ikr}}{4\pi r} \left[\left(\hat{\theta}\hat{\theta} + \hat{\phi}\hat{\phi} \right) \cdot \int \mathbf{J}(\mathbf{r}') e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} d\mathbf{r}' - \hat{\mathbf{r}} \times \int \widetilde{\mathbf{M}}(\mathbf{r}') e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} d\mathbf{r}' \right], \quad kr \gg 1 \end{aligned} \quad (3)$$

where $\widetilde{\mathbf{M}} = \mathbf{M}/\eta$ and η is the wave impedance of free space.

If the source dimensions are small compared to a wavelength, we could use Taylor series to expand the phasor term $e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'}$ in (3)

$$e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} = \sum_n \frac{(-ik)^n}{n!} (\hat{\mathbf{r}} \cdot \mathbf{r}')^n \approx 1 + (-ik)(\hat{\mathbf{r}} \cdot \mathbf{r}') \quad (4)$$

where the first-order Taylor expansion is employed. Consequently, the current integral is approximated as

$$\int \mathbf{J}(\mathbf{r}') e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} d\mathbf{r}' \approx \int \mathbf{J}(\mathbf{r}') d\mathbf{r}' + (-ik) \int \mathbf{J}(\mathbf{r}') (\hat{\mathbf{r}} \cdot \mathbf{r}') d\mathbf{r}' \quad (5)$$

The first term of (5) is related to the electric dipole radiation

$$\int \mathbf{J}(\mathbf{r}') d\mathbf{r}' = - \int \mathbf{r}' (\nabla' \cdot \mathbf{J}(\mathbf{r}')) d\mathbf{r}' = -i\omega \int \mathbf{r}' \rho(\mathbf{r}') d\mathbf{r}' = -i\omega \mathbf{p}^e \quad (6)$$

where $\mathbf{p}^e = \int \mathbf{r}' \rho(\mathbf{r}') d\mathbf{r}'$ is the electric dipole moment. The second term of (5) correlates to the magnetic dipole and electric quadrupole radiations.

First, we can split the integrand into a symmetric and antisymmetric parts

$$(\hat{\mathbf{r}} \cdot \mathbf{r}') \mathbf{J} = \frac{1}{2} [(\hat{\mathbf{r}} \cdot \mathbf{r}') \mathbf{J} + (\hat{\mathbf{r}} \cdot \mathbf{J}) \mathbf{r}'] + \frac{1}{2} (\mathbf{r}' \times \mathbf{J}) \times \hat{\mathbf{r}} \quad (7)$$

Then, we find the antisymmetric part can be expressed by magnetic dipole moment

$$\int \frac{1}{2} (\mathbf{r}' \times \mathbf{J}) \times \hat{\mathbf{r}} d\mathbf{r}' = -\hat{\mathbf{r}} \times \mathbf{m} \quad (8)$$

where $\mathbf{m} = \frac{1}{2} \int \mathbf{r}' \times \mathbf{J}(\mathbf{r}') d\mathbf{r}'$ is the magnetic dipole moment. Next, the symmetric part can be expressed by electric quadrupole moment tensor

$$\begin{aligned} & \frac{1}{2} \int [(\hat{\mathbf{r}} \cdot \mathbf{r}') \mathbf{J}(\mathbf{r}') + (\hat{\mathbf{r}} \cdot \mathbf{J}(\mathbf{r}')) \mathbf{r}'] d\mathbf{r}' \\ &= \frac{1}{2} \int (\mathbf{r}' \mathbf{J}(\mathbf{r}') + \mathbf{J}(\mathbf{r}') \mathbf{r}') \cdot \hat{\mathbf{r}} d\mathbf{r}' \\ &= \frac{-i\omega}{2} \int \rho(\mathbf{r}') \mathbf{r}' \mathbf{r}' d\mathbf{r}' \cdot \hat{\mathbf{r}} = \frac{-i\omega}{6} \overline{\mathbf{Q}}^e \cdot \hat{\mathbf{r}} \end{aligned} \quad (9)$$

where $\overline{\mathbf{Q}}^e = \int (3\mathbf{r}' \mathbf{r}' - r'^2 \bar{\mathbf{I}}) \rho(\mathbf{r}') d\mathbf{r}'$ is the electric quadrupole moment tensor. Finally, the current integral can be rewritten as a summation of electric dipole, magnetic dipole, and electric quadrupole terms

$$\begin{aligned} \int \mathbf{J}(\mathbf{r}') e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} d\mathbf{r}' &\approx \mathbf{J}_{ed} + \mathbf{J}_{md} + \mathbf{J}_{eq} \\ &= -i\omega \mathbf{p}^e + ik\hat{\mathbf{r}} \times \mathbf{m} - \frac{k\omega}{6} \overline{\mathbf{Q}}^e \cdot \hat{\mathbf{r}} \end{aligned} \quad (10)$$

Based on the dual principle, we have a similar expression for the magnetic current integral, i.e.

$$\begin{aligned} \int \mathbf{M}(\mathbf{r}') e^{-ik\hat{\mathbf{r}} \cdot \mathbf{r}'} d\mathbf{r}' &\approx \mathbf{M}_{md} + \mathbf{M}_{ed} + \mathbf{M}_{mq} \\ &= -i\omega \mathbf{p}^m + ik\hat{\mathbf{r}} \times \mathbf{m}^e - \frac{k\omega}{6} \overline{\mathbf{Q}}^m \cdot \hat{\mathbf{r}} \end{aligned} \quad (11)$$

Supplementary Note 2: Power Conversion Efficiency of the Nonlinear Nanoantenna

The power conversion efficiency (η) of the nonlinear nanoantenna is defined as the output radiation power (P_o) at the second-harmonic frequency over the input power at the fundamental frequency (P_i).

$$\eta = \frac{P_o}{P_i} = \frac{\int_s \text{Re} [\mathbf{E}^s(2\omega) \times \mathbf{H}^s(2\omega)] \cdot d\mathbf{S}}{\int_s \frac{|\mathbf{E}^i(\omega)|^2}{Z} dS} \quad (12)$$

where $Z = 120\pi$ is the wave impedance of free space. The effective focus area of laser is set to be $2 \text{ um} \times 2 \text{ um}$. **Figure S1** shows the power conversion efficiency of the nonlinear nanoantenna. From the figure, under a high input power ($P_i > 10^5 \text{ W}$) condition, pump depletion effect should be taken into account.

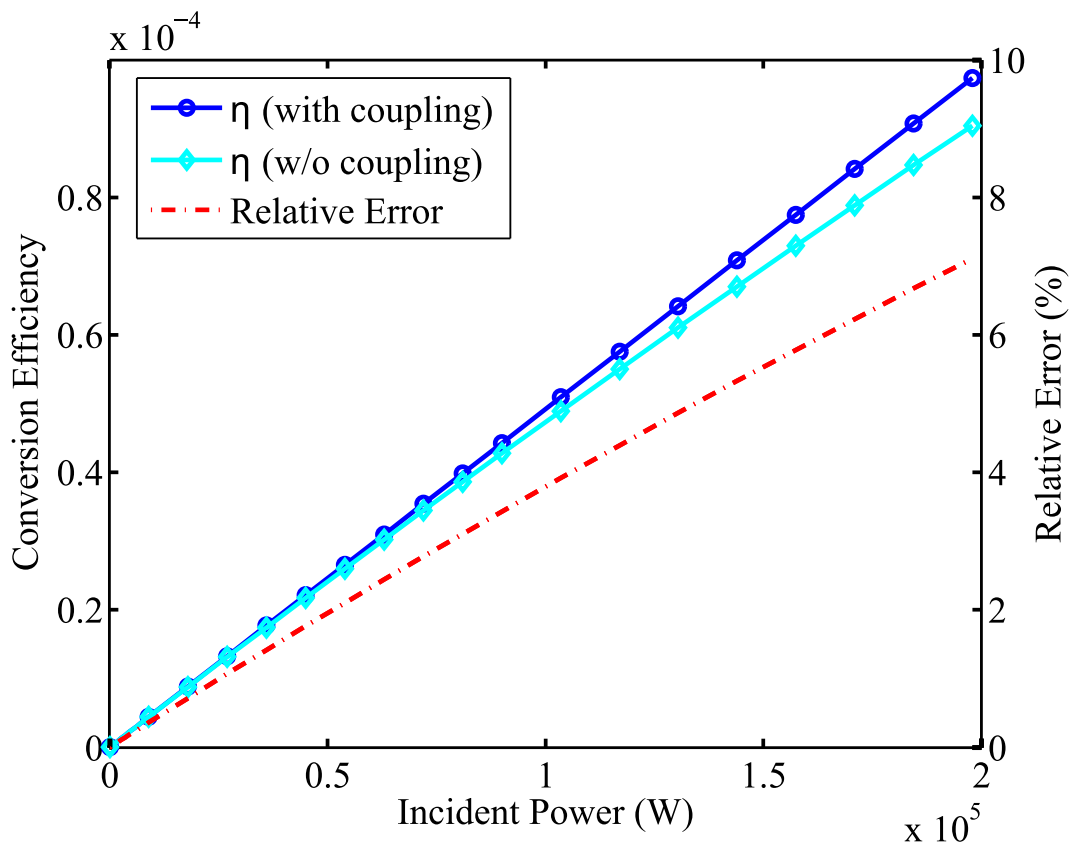


Figure 1: Power conversion efficiency of the nonlinear spherical nanoantenna. The undepleted pump approximation (w/o coupling case) is inaccurate under a high input power condition.